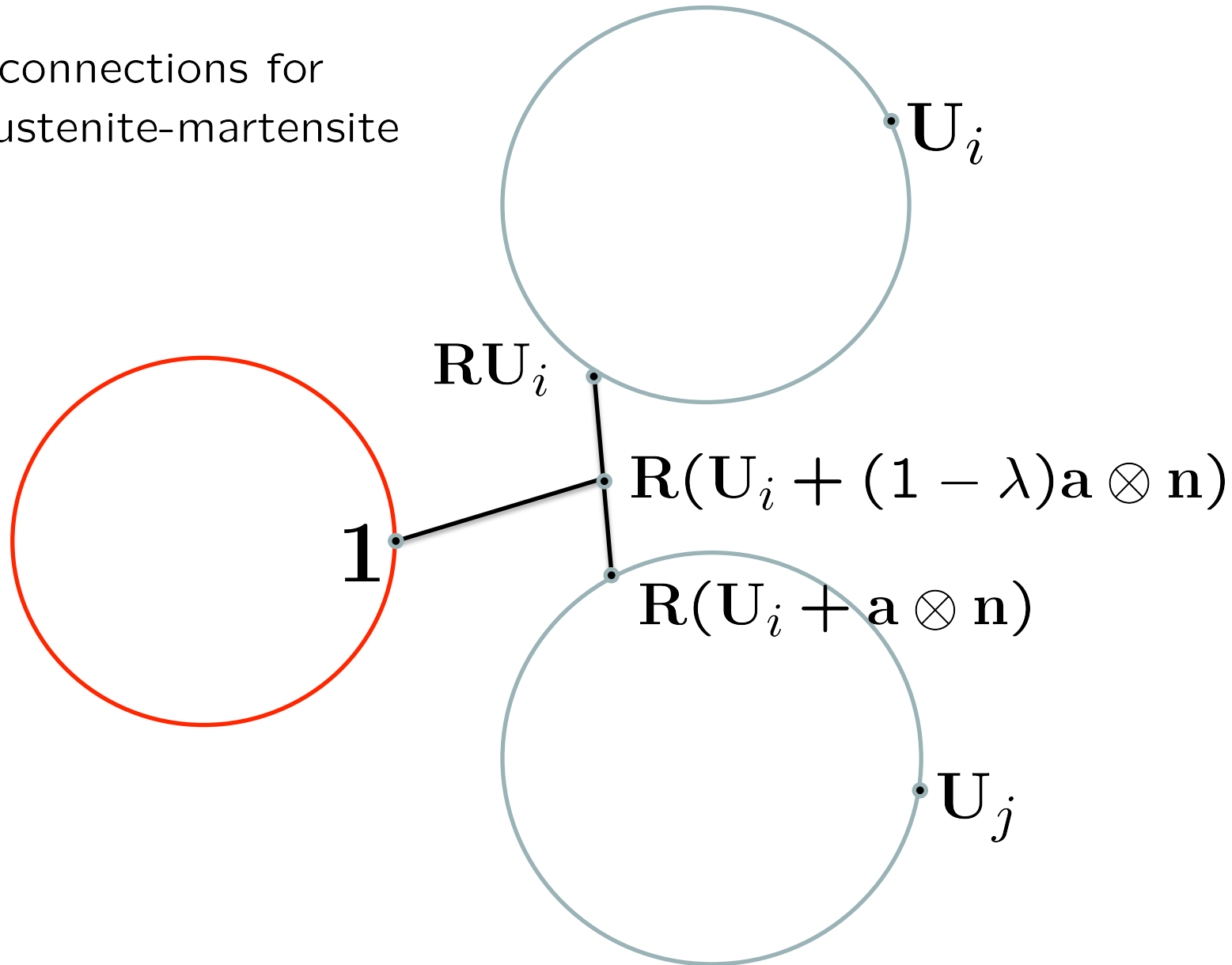


(Classical) austenite-martensite interface in CuAlNi
 (courtesy C-H Chu and R. D. James)

Rank-one connections for
classical austenite-martensite
interface



We have to solve

$$\mathbf{R}(\mathbf{U}_i + (1 - \lambda)\mathbf{a} \otimes \mathbf{n}) - \mathbf{1} = \mathbf{b} \otimes \mathbf{m}$$

for $\mathbf{R} \in SO(3)$, $\lambda \in [0, 1]$ and $\mathbf{b}, \mathbf{m} \in \mathbb{R}^3$.

The solutions (JB/James 1987) give the formulae of the *crystallographic theory of martensite* (Wechsler, Lieberman & Read 1953)

Let $\delta^* = \mathbf{a} \cdot \mathbf{U}_i (\mathbf{U}_i^2 - \mathbf{1})^{-1} \mathbf{n}$.

Case 1. If \mathbf{U}_i does not have an eigenvalue 1 then there is a solution iff $\delta^* \leq -2$ and

$$\text{tr } \mathbf{U}_i^2 - \det \mathbf{U}_i^2 - 2 + \frac{1}{2\delta^*} |\mathbf{a}|^2 \geq 0,$$

and if $\delta^* < -2$ there are exactly four solutions

$$\begin{aligned} & (\mathbf{R}_1, \lambda^*, \mathbf{b}_1^+ \otimes \mathbf{m}_1^+), & (\mathbf{R}_2, \lambda^*, \mathbf{b}_1^- \otimes \mathbf{m}_1^-), \\ & (\mathbf{R}_3, 1 - \lambda^*, \mathbf{b}_2^+ \otimes \mathbf{m}_2^+), & (\mathbf{R}_4, 1 - \lambda^*, \mathbf{b}_2^- \otimes \mathbf{m}_2^-), \end{aligned}$$

where $\lambda^* = \frac{1}{2} \left(1 - \sqrt{1 + \frac{2}{\delta^*}} \right)$.

Case 2. There are solutions for every $\lambda \in [0, 1]$ iff the following *cofactor conditions*

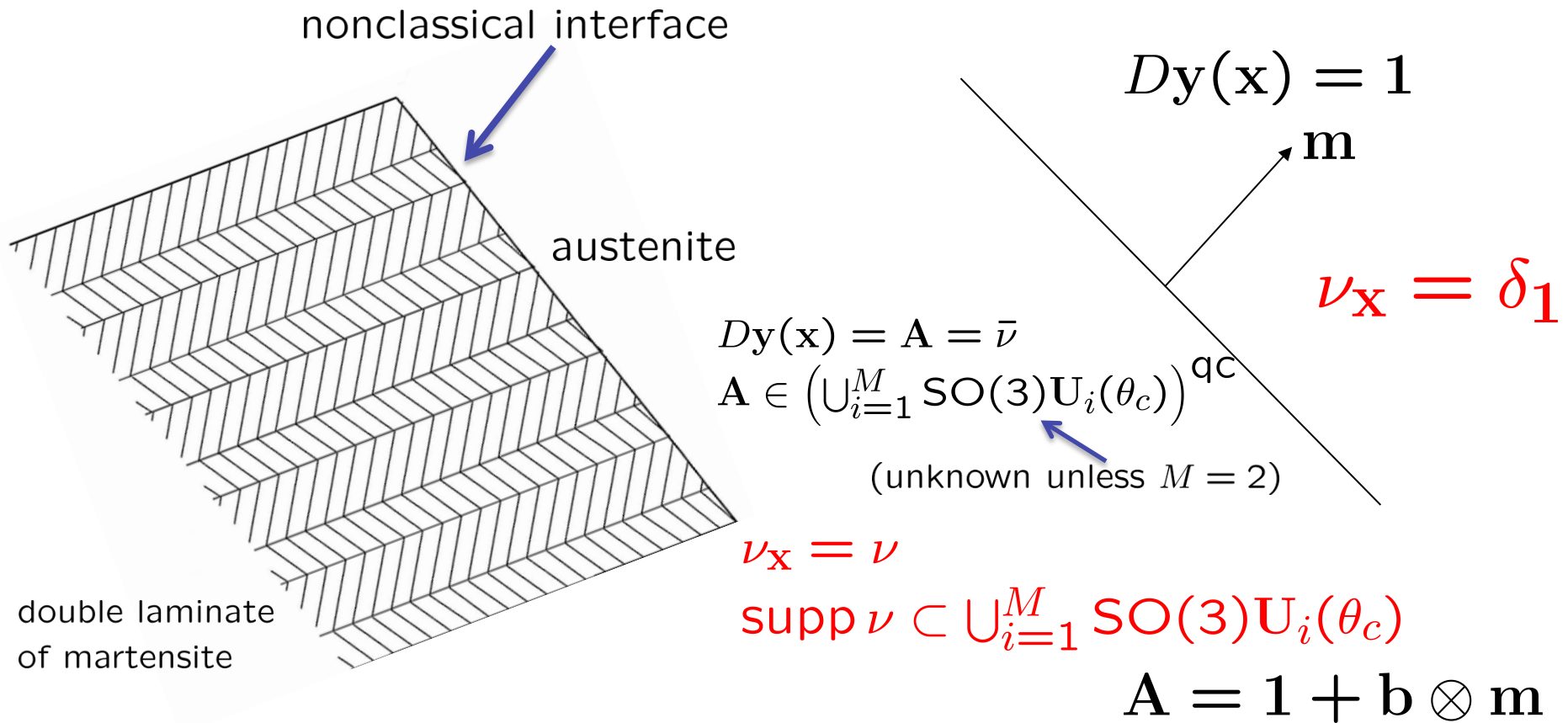
U_i has middle eigenvalue 1

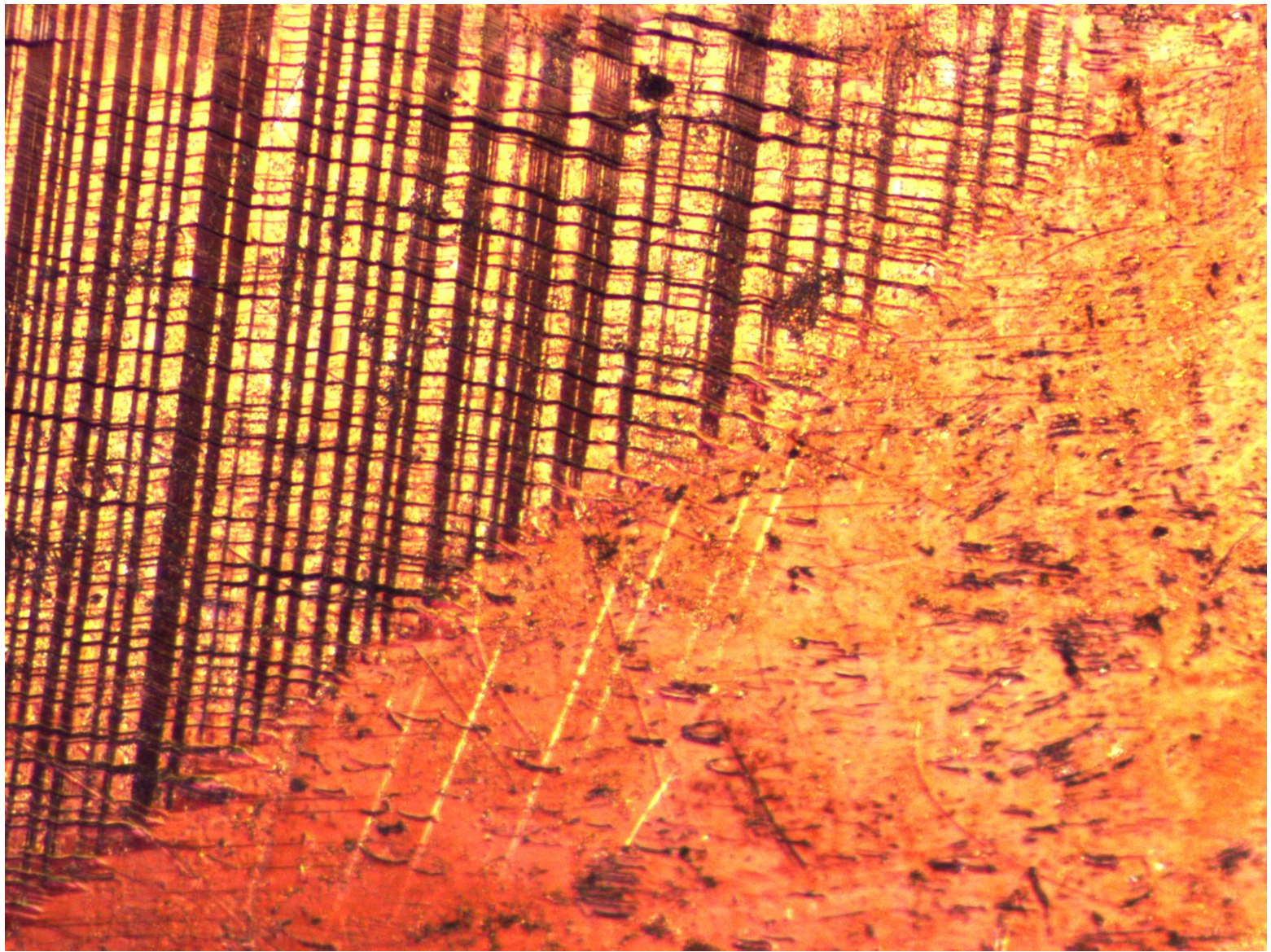
$$\mathbf{a} \cdot \text{cof}(U_i^2 - \mathbf{1})\mathbf{n} = 0,$$

$$\text{tr } U_i^2 - \det U_i^2 - \frac{|\mathbf{a}|^2}{4} - 2 \geq 0$$

hold.

But why (cf JB/Carstensen 1997) should the martensitic microstructure be a simple laminate, rather than something more complicated, such as a double laminate?

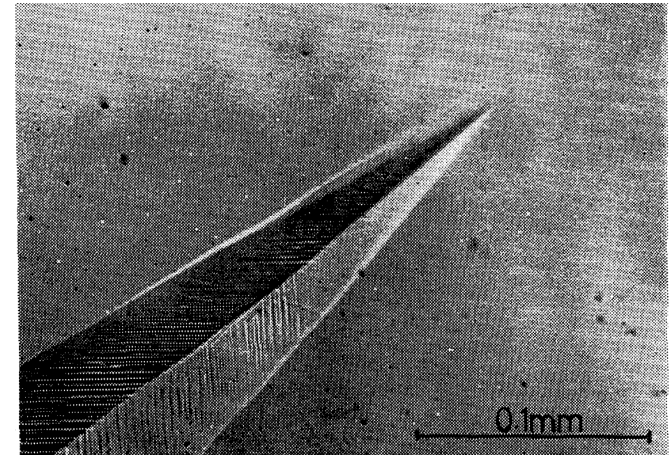
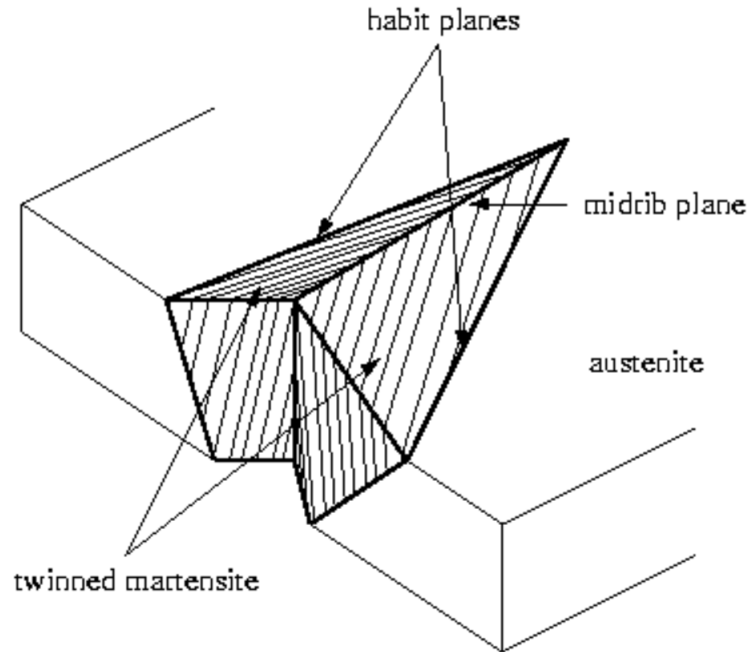




Nonclassical austenite-martensite interface in CuAlNi (H. Seiner)

Special compositions and the discovery of low hysteresis alloys.

1. The wedge microstructure (Bhattacharya 1991)



Wedge microstructure in CuAlNi
Otsuka & Shimizu (1969)

Microstructure supported on energy wells impossible for cubic-to-tetragonal, possible for cubic to orthorhombic iff the eigenvalues α, β, γ of the transformation strain $U_i(\theta_c)$ satisfy a special relation $f(\alpha, \beta, \gamma) = 0$, which holds to high accuracy for the actual compositions close to Cu-14.2wt.%Al-4.3wt.%Ni used in shape-memory alloys.

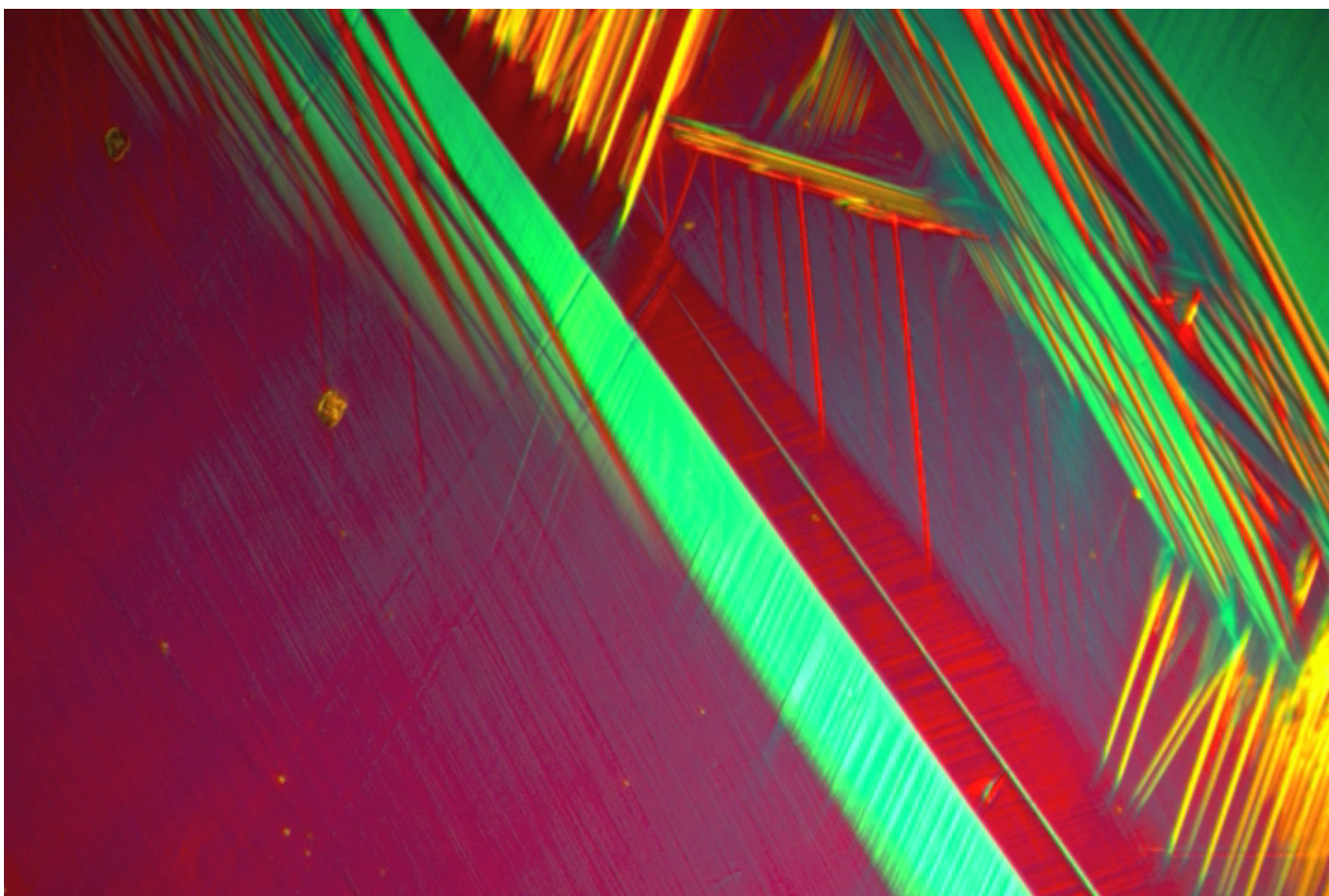
2. Ultra-low hysteresis alloys

James *et.al.* (2013) tuned the composition of a ZnAuCu alloy so that the cofactor conditions were very nearly satisfied, with dramatic results.

(i) the thermal hysteresis was reduced from typical values of $50^{\circ} - 70^{\circ}\text{C}$ to about 2°C .

(ii) Material undamaged after thousands of thermal cycles (millions for a material discovered later by Quandt, Wuttig et al 2014).

(iii) During thermal cycling remarkable martensitic microstructures are observed that are completely different in each cycle.



Zn₄₅Au₃₀Cu₂ ultra-low hysteresis alloy Song, Chen, Dabade, Shield, James, 2013
‘Moving mask’ approximation analyzed by Della Porta (2018), who has also identified further conditions on the \mathbf{U}_i allowing new microstructures, closely satisfied in this alloy.